CO₂ Reduction

Comparison of Belt and Chain Front End Drive for a Passenger Car High Pressure Pump

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High Pressure Pump Drive



- Fuel Economy Direct contribution
 - Parasitic losses
 - Friction and Damping losses
 - Hub loads and bearing losses
- Fuel Economy Indirect contribution
 - Injection Dynamics
 - Torque oscillation
 - Drive elongation
 - Damping of C/S torsional vibrations
 - Pressure build-up rate in common rail







Hydraulics & Mechanics



Conventional simulation

- Mechanic model excited by imposed delivery pressure profile on plunger or torque measured data
- Hydraulic simulation with imposed rigid motion of plunger or pulley

Integrated model

- Hydraulic and Mechanic co-simulation
- Pressure build-up function of computed elastic motion of plunger
- Mechanical model excitation through simulated pressure at plunger
- Interaction allowed
- Imposed crankshaft motion, including torsional vibrations





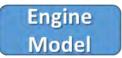


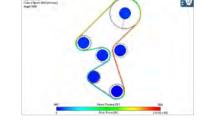
Simulation Methodology



- Mechanical Model VALDYN
 - Detailed pump dynamic model
 - Used worldwide since decades for belt and chain drive modeling
- Hydraulic model AMESim
 - Developed by Bosch
 - Modified to be integrated into a cosimulation;
- Parent Model Simulink
 - Monitors passage of results between models
 - Coordinates computation time
 - Uses co-simulation libraries available in both environments





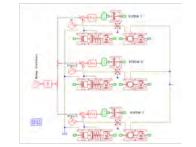














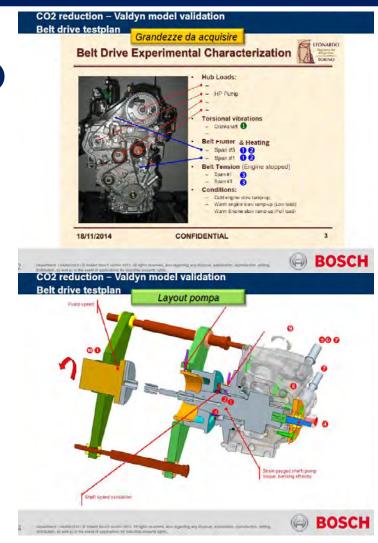


Validation methodology



- Three sources of experimental data (belt)
 - HPP torque measurement @ test rig;
 - Instrumented HPP on engine @ OEM production plant;
 - Specific engine test at Bosch CVIT
- Specific instrumentation for:
 - Belt slap
 - HPP hub load and torque
 - HPP housing vibration
 - Injection system characterization (low and high pressure circuits)







Pump Model



• Cam – Roller contact

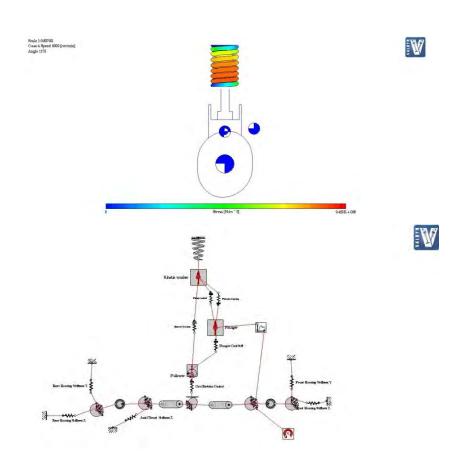
- EHD Theory for oil film thickness and friction coefficient assessment
- Fuel piezo-viscosity parameters
- Statistic asperity contact model to define friction torque (GWT model)
- Retainer spring modeled

• Spring

- Multi-mass model (10 segments per coil)
- Coil contacts and coil surge modeled

• Shaft

- Two flexible elements
- Two pivot bearing with constant friction coefficient;
- In the complete model with belt, an additional front cantilever part and toothed pulley are included







Pump Model Validation



Two Phases

- Preliminary
 - Stand-alone model, imposed pressure profile from previous injection system simulation;
 - Compared with available pump test rig data;
 - Use to validate torque and friction behavior

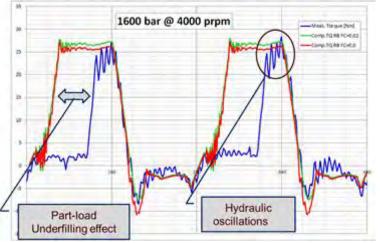
Final

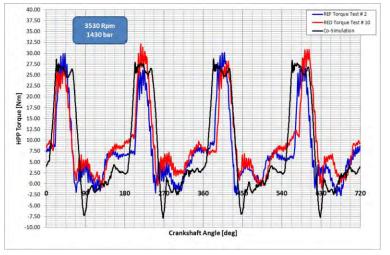
- Complete model with belt drive
- Integration with hydraulic model
- Compared with engine *ad-hoc* measurements

Model evolution

• @ part load the throttling of the pump by the Metering Unit can be predicted only with the integrated model











Belt Model



Model

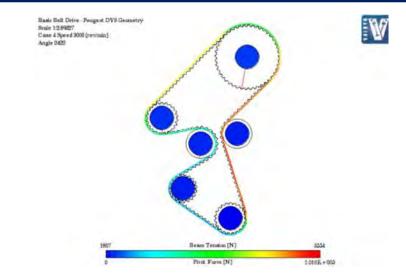
- Succession of beams with profiles entering the grooves of the pulleys
- Both contact friction and internal damping modeled
- Automatic pivoting tensioner

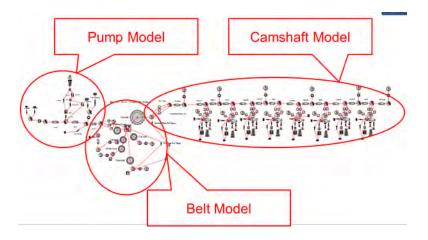
• Layout

• Corresponding to an engine available for tests and on which past engineering experience was available

Components

- Direct information from suppliers was not available
- Information derived from purchased spare parts
- Single camshaft and valve drive included
- Belt lay-out specific and derived from existing lay-outs
- Information collected either from spare parts and experimental results









Chain Model



Model

 Series of partially elastic links with both friction and damping at elements' interface

• Lay-out

- Designed from scratch
- Concept derived from an existing engine

Lower Chain

- Step 9,525 mm
- 72 links
- 25 teeth sprockets
- Specs: IWIS G68 HR-4

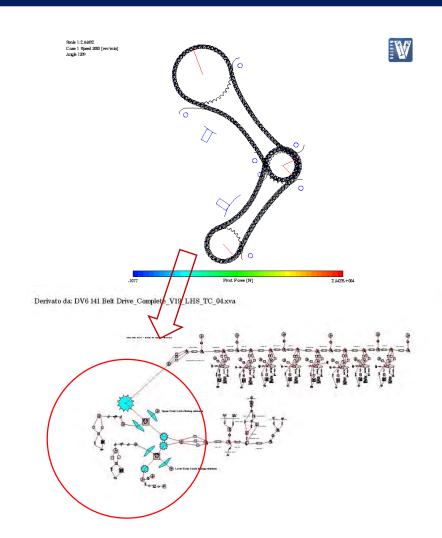
Upper Chain

- Step 9,525 mm
- 90 links
- 21/42 teeth sprockets
- Specs: IWIS G67 HR-6

Camshaft

• Model with one single camshaft to allow for direct comparison with belt drive







Chain Model Optimization

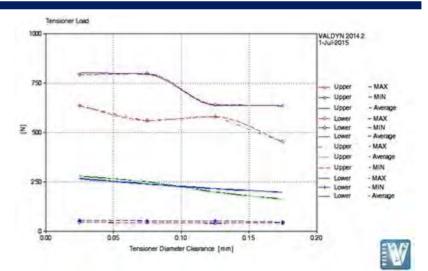


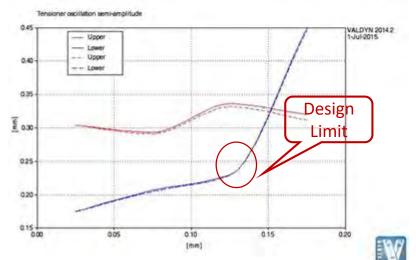
Parameters

- Tensioners preload
- Tensioners leakage
- Guide friction

Criteria

- Minimum friction in dynamically stable conditions
- Minimum attainable friction coefficient for guides









Hydraulic Model Integration



Hierarchy

- Simulink model is parent to both VALDYN and AMESim models
- S/link coordinates both time step definition and synchronization

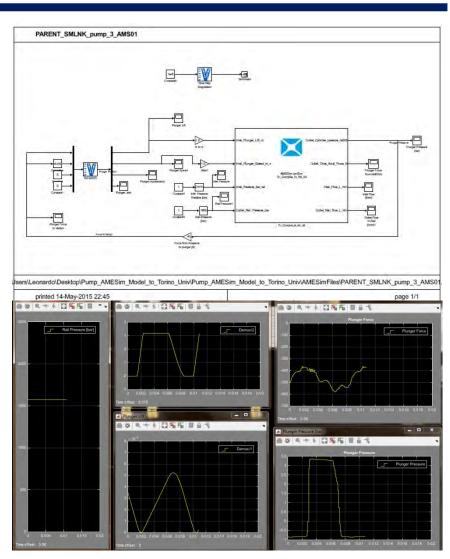
Visualization

• Simulink terminals allow for constant monitoring of the run

Simulation time

- Approx. 5 engine cycles to achieve convergence
- Elapsed time: 6h to 8h

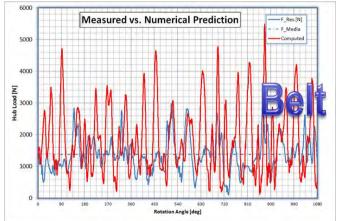






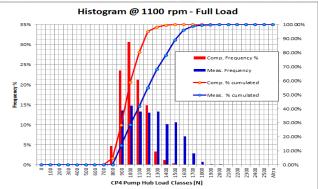
Belt Model Validation

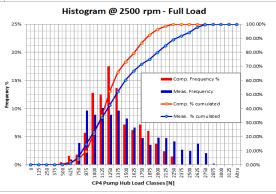


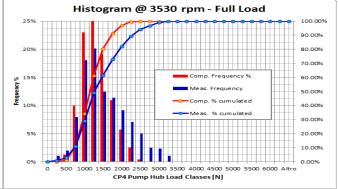


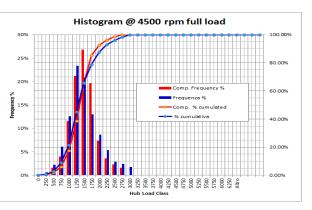
Hub Load Comparison

- Very dispersed results both in numerical and experimental results, no cyclic repetition;
- Comparison of frequency distribution curve is used;
- Very good matching at various speed is obtained after tuning of tensioner characteristics;











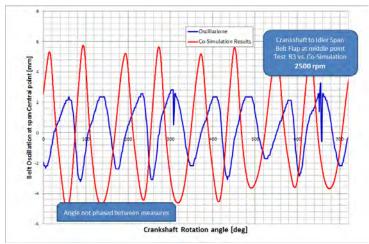


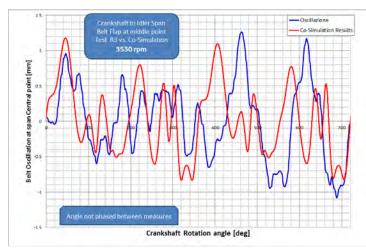
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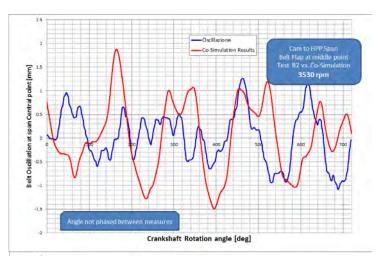


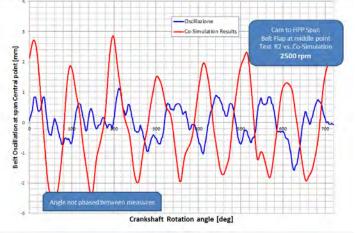
Belt flap Comparison

- Simulation results matched HSC measurements in a fair good fashion by different speeds;
- Computed amplitudes generally exceeded measured ones, showing a lower damping than real;
- Finer definition of belt characteristic for future simulation can be envisaged;











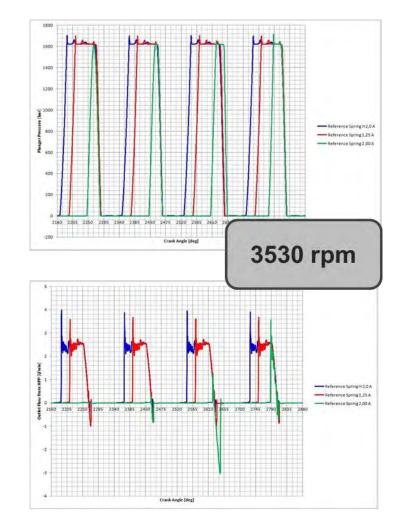


Simulation Results



Part Load operation

- Changes at Metering Unit current correctly result in a lower filling quote of the delivery plunger;
- This effect can be seen both on the plunger pressure curves and in the flow out of the delivery valve
- Note zero delivery situation at high throttling;







Simulation Results



Parasitic Losses

- Power absorption higher for chain drive
- Optimization could reduce difference but not reverse the result;
- Belt Losses mainly from internal damping, increase with speed and affected by resonances
- Chain drive main contribution from friction
- High speed gasoline engine may experience opposite results;



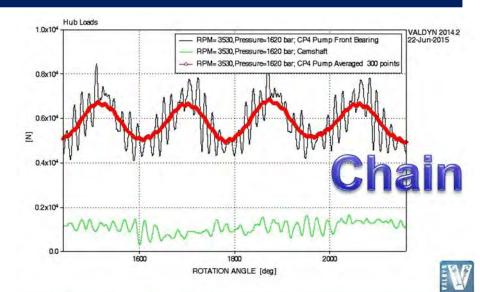


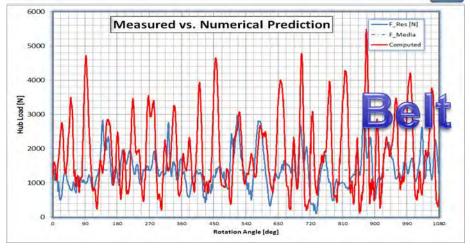


Simulation Results



- Dynamic Behavior
 - Belt:
 - Mainly stochastic behavior, oscillation overwhelms cyclic load
 - Chain:
 - Clearly cyclic repeatable oscillation
 - Two predominant frequency:
 - High frequency teeth meshing
 - Low frequency energy bouncing due to elastic behavior of the drive







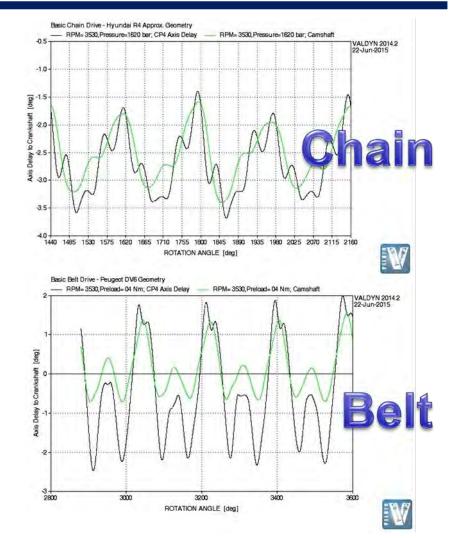


Pump Dynamics



Phase shift

- Higher belt deformation lead to higher phase shifts
- HPP pump torque oscillation is the driving force
- Such phase shift appears to have no significant influence on injections parameters in a HPCR Systems





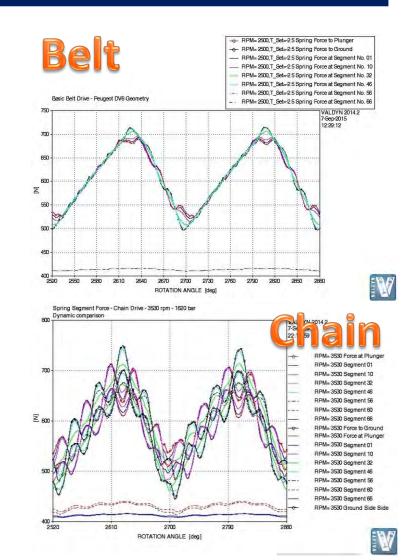


Main pump spring surge



Spring dynamics

- Forces at different portions of spring coils have been analyzed
- Oscillation around static force is a consequence of the excitation of spring modal frequencies
- The repeatable chain meshing frequency excites spring surge at certain speeds
- Belt drive influence on spring dynamics is negligible





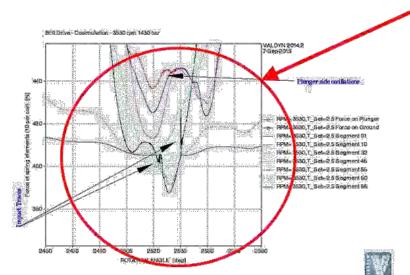


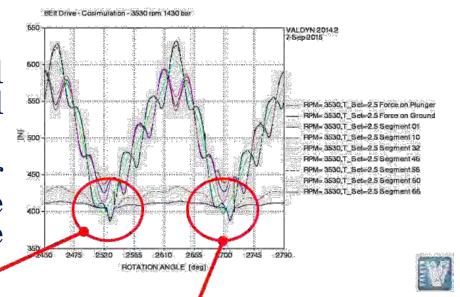
Main pump spring surge

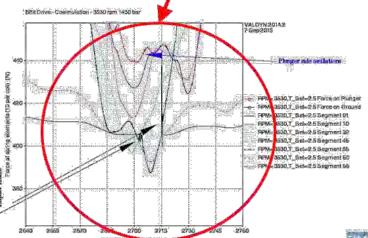


• Spring surge (Chain Drive)

- Spring coil oscillation near spring basis lead to impingements of the first coil with dead ones
- Such impingement might result into higher vibration level of the HPP housing, hence structure borne noise and delivery pressure oscillation.













Summary and Conclusions



Simulation

• Use of different codes co-simulation can efficiently deepen the analysis into the dynamics of injection system unveiling interaction between mechanical and hydraulic engineering aspects;

Chain vs. Belt Front End drive

- For high speed diesel engines for passenger car, a belt drive shows marginal advantages in friction reduction;
- Chain dynamics may have an impact on secondary dynamics of HPP components, in particular on the return spring dynamics





Q & A session



Q&A







Thank you

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